





Highly Variable Radiators for Improved Spacecraft Thermal Control

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- Spacecraft (SC) must be kept within proper temperatures
- High power SC in Earth orbit need to reject waste heat
- Deep space exploration missions need to both reject excess heat and conserve heat in different mission phases
- Variable radiators provide this capability.



Variable louver radiator on Juno.



- Variable heat rejection is an enabling technology to reliably vary heat rejection during human and robotic spaceflight missions with wide variation in thermal environments and vehicle heat loads
- Technology advancements needed include variable heat rejection radiators, with low mass and high energy efficiency



SMM4 with louver radiators.



- Spacecraft waste heat is rejected to space by radiators
- Heat leaves the SC and radiator via blackbody radiation

$$Q = A \cdot \varepsilon \cdot \sigma \cdot (T_{hot}^4 - T_{cold}^4)$$

- SC internal heat is currently brought to radiator surface via heat doublers, heat pipes or pumped coolant loops
- Variable radiators use variable emissivity coatings or surfaces, variable surface area, or pumped loops.



High power deployed radiators on ISS use pumped NH_3 loops.



- Current state-of-the-art variable radiators are louver design
- Movable louvers cover/uncover a high ε surface with metal vanes of low ε
- Effective ε varies from 0.14 to 0.7, for a 5:1 *turndown* ratio
- NASA has requested new technology able to provide
 6:1 to 12:1 *turndown* ratios



Louver radiator design.

Multiple louver radiators on Rosetta.



Integrated Multilayer Insulation (IMLI)



- Ball Aerospace and Quest Thermal Group have been developing advanced thermal insulation systems since 2007
- IMLI is an advanced next generation MLI
- Uses discrete polymer spacers instead of netting
- IMLI has half the heat flux per layer of netting MLI
- IMLI has predictable thermal performance
- IMLI and variants provide structural support up to 90 psi



IMLI showing spacers and layers.



IMLI flight on GPIM & RRM3

- Green Propellant Infusion Mission (GPIM)
 - NASA and Ball Aerospace & Technologies
 Corp. are collaborating on GPIM
 - Will demonstrate the capabilities of a Hydroxyl Ammonium Nitrate fuel/ oxidizer
 - Flight scheduled for June 2019
- Remote Refueling Mission 3 (RRM3)
 - NASA RRM3 flight experiment on cryogenic storage and transfer
 - IMLI insulates a cryocooled flight dewar
 - IMLI flew on CRS-16, is currently on the ISS, and is at TRL9







A family of insulation systems have evolved based on Discrete Spacer Technology





	Application	Development Status	TRL
Integrated Multilayer Insulation (IMLI)	In space and high vacuum	Phase 3 SBIR completed, 1 st spaceflight 2018	9
Load Bearing Multilayer Insulation (LBMLI)	Supports thermal shields for active cooled systems	Phase 3 SBIR completed	5
Vapor Cooled Structure MLI (VCSMLI)	Vapor cools tank support elements	Phase II SBIR complete	5
Cellular Load Responsive MLI (CLRMLI)	Replaces SOFI on launch vehicle cryotanks	Phase II SBIR complete	4
Vacuum Cell Multilayer Insulation (VCMLI)	Replaces SOFI on launch vehicle cryotanks	Phase I CRAD complete	4
Multi-Environment MLI (MEMLI)	Operates in environments from space to on-Mars	Phase II SBIR in progress	4
Micrometeorite and Orbital Debris MLI (MMOD MLI)	Thermal insulation and MMOD protection	Phase I SBIR complete	3
Variable Conductance Radiator Variable Gas Radiator	Spacecraft thermal control	Phase II SBIR in progress	4

Control over internal pressures



- Quest Thermal and Ball have developed systems that control internal gas pressures or internal vacuum - useful for Variable Gas Radiators.
- Cellular Load Responsive MLI and Vacuum Cell MLI use a cellular core that cryopumps internal gas species, has internal or external IMLI layers, and performs both in-air and in-space.



VCMLI left, CLRMLI concept (middle); CLRMLI prototype (right)



- Variable Conductor Radiator uses variable heat actuators embedded in IMLI insulation
- Heat conductors are SMA actuators that open/close thermal paths
- VCR is capable of acting as either high performance insulation or an effective radiator



SMA actuators compress the conductive pillars, forming high heat conductive paths through the VCR. Closed conductors provide high heat transfer to the radiator outer surface.



- VCR can be engineered for specific heat rejection values
- Number of IMLI layers affects minimum and maximum heat radiated
- Heat actuators can be varied for size, number and interface conductance
- Thermal modeling estimates high turndown ratios are possible.

Variable heat rejection, number of radiation shield layers, and turndown ratios with 2 - 5 layers.

# Radiation Shield Layers	Warm Boundary	Cold Boundary	No conductors W/m ²	All conductors W/m ²	Turndown ratio
2	295 K	3 K	9.1	383	42
3	295 K	3 K	4.7	376	80
5	295 K	3 K	2.3	368	160

Modeled maximum and minimum heat rejection.

- A VCR prototype was modeled, analyzed, designed, built and tested in an SBIR Phase I
- Heat actuators were designed and demonstrated to work (SMA and bimetallic passive actuators).
- Heat radiated varied from 24.9 W/m² to 268 W/m², achieving a turndown ratio of 11:1

Minimum VCR	Maximum VCR
Radiated Heat	Radiated Heat
@ 283K	@ 363K
2.32W	24.9W
24.9 W/m ²	268 W/m ²
R Turndown ratio	Measured 11:1





VCR

V

- Variable Conductor Radiator technology was proven feasible and achieved TRL4
- Heat flows were analyzed; next generation actuator design should improve maximum and minimum heat radiated
- A 31:1 or greater turndown ratio is modeled and believed achievable

Minimum VCR	Maximum VCR	Maximum Modeled
Radiated Heat	Radiated Heat	Radiated Heat
@ 283K	@ 363K	@ 363K
2.32W	24.9W	
24.9 W/m ²	268 W/m ²	788 W/m ²
VCR Turndown ratio	Measured 11:1	Modeled 31:1

VCR heat actuators f backplane film heaters.





Variable Gas Radiator (VGR)



- VGR uses variable gas conductance within an IMLI insulation stack
- VGR can also act as either a good insulator or a good radiator



Variable Gas Radiator



- VGR heat conduction through the Variable Radiator is controlled by the number of IMLI layers, gas species, gas pressure, emissivity of outer radiator surface, and parasitic heat leak
- Modeled max and min heat rejection shown below
- VGR should be capable of high turndown ratios



IMLI layers can be varied to control max/min heat flow

Modeled VGR Heat Rejection					
# IMLI radiation shields	Warm Boundary	Cold Boundary	Internal Vacuum W/m²	He Gas Filled W/m ²	Turndown ratio
2	295 K	3 K	9.1	378	<mark>41</mark>
3	295 K	3 K	4.7	358	<mark>76</mark>
5	295 K	3 K	2.4	325	<mark>136</mark>
10	295 K	3 K	1.1	267	<mark>248</mark>

Variable Gas Radiator



- Heat conduction through radiator controlled by gas pressure
- Pressures in the range 0.1 millitorr to 1 torr allow full heat control
- Low level precision gas pressure controller was developed

Helium gas pressure torr	Vacuum	0.0001	0.001	0.01	0.1	1	10
Modeled Radiated heat (W)	9.11W	10.1W	17.9W	66.1W	218W	377W	377W
%Max Heat Flux	2%	3%	5%	18%	58%	100%	100%
Radiator Surface Temp, K	114	117	135	187	252	289	289
BaseplateTemp, K	294	294	294	294	294	294	294





Variable Gas Conductor Radiator

- A VGR prototype was designed, built and tested
- A gas enclosure was designed and fabricated
- Radiator test platform was designed and built





VGR prototype ready for test; left two images show prototype mounted and facing cold target; right images show VGR outer radiator surface fabrication









Variable Gas Conductor Radiator



Radiated heat was controlled by gas pressure and baseplate temperature

Baseplate temperature °C	Gas pressure torr	Radiated Heat Flux W/m ²
10 °C	0.000	7.86
10 °C	0.050	97.05
10 °C	0.100	125.7
10 °C	0.500	199.0
10 °C	1.000	216.2
40 °C	0.050	116.6
40 °C	0.100	139.5
40 °C	0.500	252.6
40 °C	1.000	283.2

VGR Measured Radiated Heat



Heat Flux Values <u>vs</u> gas pressure at 10C and 40C

VGR radiated heat flux	'off'	283K	7.86 W/m ²
	'on'	313K	283 W/m ²

Turndown ratio: 36:1

Variable Gas Conductor Radiator



- Variable Gas Radiator technology was proven feasible, reached TRL4
- A first prototype achieved a 36:1 turndown ratio
- Good agreement between thermal model and test data
- Lightweight system at 0.69 kg/m² (louvers are ~5 kg/m²)
- NASA SBIR Phase II R&D program in progress
- 2nd generation VGR has improved enclosure, gas control, and larger expected turndown ratio
- Current R&D is to mature and improve Variable Radiator technologies

	Turned off	Turned fully on	Turndown ratio	
VGR modeled heat flux	9.1 W/m ²	377W/m ²	41:1	
VGR measured heat flux	7.9 W/m ²	283W/m ²	36:1	

Variable Radiator technologies



- Variable Radiator technology, using either variable heat actuators or variable gas controllers, was proven feasible, and are at TRL4
- First prototypes achieved 11:1 to 36:1 turndown ratios
- Thermal model and prototype test data suggest much higher turndown ratios can be achieved
- R&D work is in progress, funded by NASA SBIR program
- R&D goals are to mature and improve Variable Radiator technologies, and prepare for commercial availability



VGR left, VCR right.

